

Thermal Physics Meeting VIII I

- I Last time
- II Macroscopic determination of quantities W, E, Q, T .
- III Heat capacity and specific heat
- IV Macro determination of entropy

$$kT \approx \frac{E}{S}$$

$$\frac{\Delta E}{E} = \frac{1}{\sqrt{S}}$$

$$\bar{X} = \frac{1}{\beta} \frac{\partial \ln Z}{\partial x}$$

$$\beta = \frac{\partial \ln Z}{\partial E}$$

Equations of state.

II If we only have access to macroscopic parameters how do we measure them? And how do we characterize a system with them?

Work: If a quasi-static process takes V_i to V_f then

$$W = \int_{V_i}^{V_f} P(V) dV$$

Work done by system

Internal Energy Thermally insulated. Then

$$Q = 0 \text{ and}$$

$$\Delta E = -W$$

$$E_b - E_a = -W_{ab} = -\int_a^b P dW$$

As always we are free to choose our zero of energy. For convenience choose experimentally easy state $E_a = 0$.

Then $E_b = -W_{ab}$

Heat: We have also shown

$$Q_{ab} = \Delta E + W_{ab} = E_b - E_a + W_{ab}$$

⇒ gives Q_{ab} .

Various ways of achieving this in practice - important but more practical to study in context.

Keeping V fixed and measuring \bar{P} gives you access to T .

III Not all systems respond to having heat added in the same way - feet on cold tile vs, feet on carpet.

The heat capacity is a way to capture these differences

$$(dQ)_y = C_y dT)_y$$

(Absolute) Temperature:

P2/4

Using an equation of state
[Recall: Equations of state relate generalized forces, external params, and temperature. Get 'em from

$$\Omega, \quad \beta = \frac{\partial \ln \Omega}{\partial E} \quad \bar{X}_r = \frac{1}{\beta} \frac{\partial \ln \Omega}{\partial x_r}$$

$$\bar{P} = \frac{1}{\beta} \frac{\partial \ln \Omega}{\partial V} \Rightarrow \bar{P}V = NkT$$

or

$$C_y = \left(\frac{dQ}{dT} \right)_y \text{ at constant } y$$

as such

$$C_y = C_y(T, y)$$

Of course, if you have more stuff it can absorb more heat. This leads to

$$C_y = \frac{1}{N} C_y = \frac{1}{N} \left(\frac{dQ}{dT} \right)_y$$

For C_p in general

$$dQ = dE + p dV$$

both internal energy increases and work is performed. This means that for a given dQ , dE changes less and hence dT is smaller. This means

$$C_p > C_v$$

Well, $Q_A + Q_B = 0$.

Now

$$dQ = m c dT$$

So $Q_A = m_A \int_{T_A}^{T_f} c_A dT = m_A c_A (T_f - T_A)$
and similarly

$$Q_B = m_B c_B (T_f - T_B)$$

So $(m_B c_B + m_A c_A) T_f = m_A c_A T_A + m_B c_B T_B$

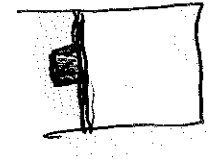
or

and

$$c_y \equiv \frac{1}{m} C_y = \frac{1}{m} \left(\frac{dQ}{dT} \right)_y$$

The dependence on y is significant.

Common case $y = V$ or $y = P$



For C_v we fix the piston, then

$$dQ = dE \quad \text{and} \quad c_v = \frac{1}{m} \left(\frac{\partial E}{\partial T} \right)_V$$

Consider a copper block of mass m_A immersed in a tank of water of mass m_B at 1 atm of pressure.

Suppose that c_A and c_B are given and for the temperatures of this

Setup $C_A(T) = \text{const}$, $C_B = \text{const}$, those temps are T_A and T_B . What is T_f ?

$$T_F = \frac{m_A C_A' T_A + m_B C_B' T_B}{(m_B C_B' + m_A C_A')}$$

Finally, we can express heat capacities in terms of entropy

$$\delta Q = T dS$$

so

$$C_y = T \left(\frac{\partial S}{\partial T} \right)_y$$

In our previous example, what is the ^{total} entropy change?

$$\begin{aligned} \Delta S_A &= S_A(T_F) - S_A(T_A) = \int_{T_A}^{T_F} \frac{m_A C_A' dT}{T} \\ &= m_A C_A' \ln \left(\frac{T_F}{T_A} \right) \end{aligned}$$

Similarly for ΔS_B and so

$$\Delta S_A + \Delta S_B = m_A C_A' \ln \frac{T_F}{T_A} + m_B C_B' \ln \frac{T_F}{T_B}$$

IV Entropy

$$dS = \frac{\delta Q}{T}$$

so

$$S_B - S_A = \int_{T_A}^{T_B} \frac{\delta Q}{T} \quad (\text{quasi-static process})$$

If we've already measured the heat capacity then

$$S(T_B) - S(T_A) = \int_{T_A}^{T_B} \frac{C_y(T) dT}{T}$$

A nifty argument shows that

$$\Delta S_A + \Delta S_B \geq 0$$

First $\ln x \leq x - 1$

$$\Rightarrow -\ln x \geq -x + 1$$

$$\Rightarrow \ln \frac{1}{x} \geq -x + 1$$

$$\text{Let } y = \frac{1}{x} \quad \ln y \geq -\frac{1}{y} + 1$$

$$\begin{aligned} \Delta S_A + \Delta S_B &\geq m_A C_A' \left(1 - \frac{T_A}{T_F} \right) + m_B C_B' \left(1 - \frac{T_B}{T_F} \right) \\ &= \frac{1}{T_F} [m_A C_A' (T_F - T_A) + m_B C_B' (T_F - T_B)] \geq 0 \end{aligned}$$